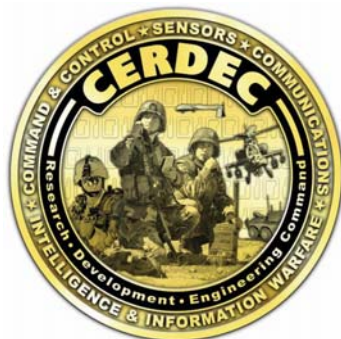


Power Generation and Alternative Energy Branch

US Army RDECOM CERDEC CP&ID Power Division

Aberdeen Proving Ground, MD



PGAE - TR - 11 - 15

Hybrid Vapor Compression Ejector Cycle: Presentation to IAPG Mechanical Working Group

Parmesh Verma and Tom Radcliff, United Technologies Research Center

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13. SUPPLEMENTARY NOTES					
14. ABSTRACT An overview of the hybrid vapor compression ejector heat pump cycle developed under an American Recovery and Reinvestment Act funded contract is provided.					
15. SUBJECT TERMS environmental control unit; ejector heat pump; vapor compression cycle					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT Same as Report (SAR)	18. NUMBER OF PAGES 15	19a. NAME OF RESPONSIBLE PERSON
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Communications-Electronics Research
Development and Engineering Center

Hybrid Vapor Compression Ejector Cycle

Final Review

Parmesh Verma and Tom Radcliff

Aug. 2011



United Technologies Research Center – East Hartford, CT

Outline

CO₂ Hybrid Vapor Compression Ejector Cycle

System Overview

Component and System Design

Integrated Controls

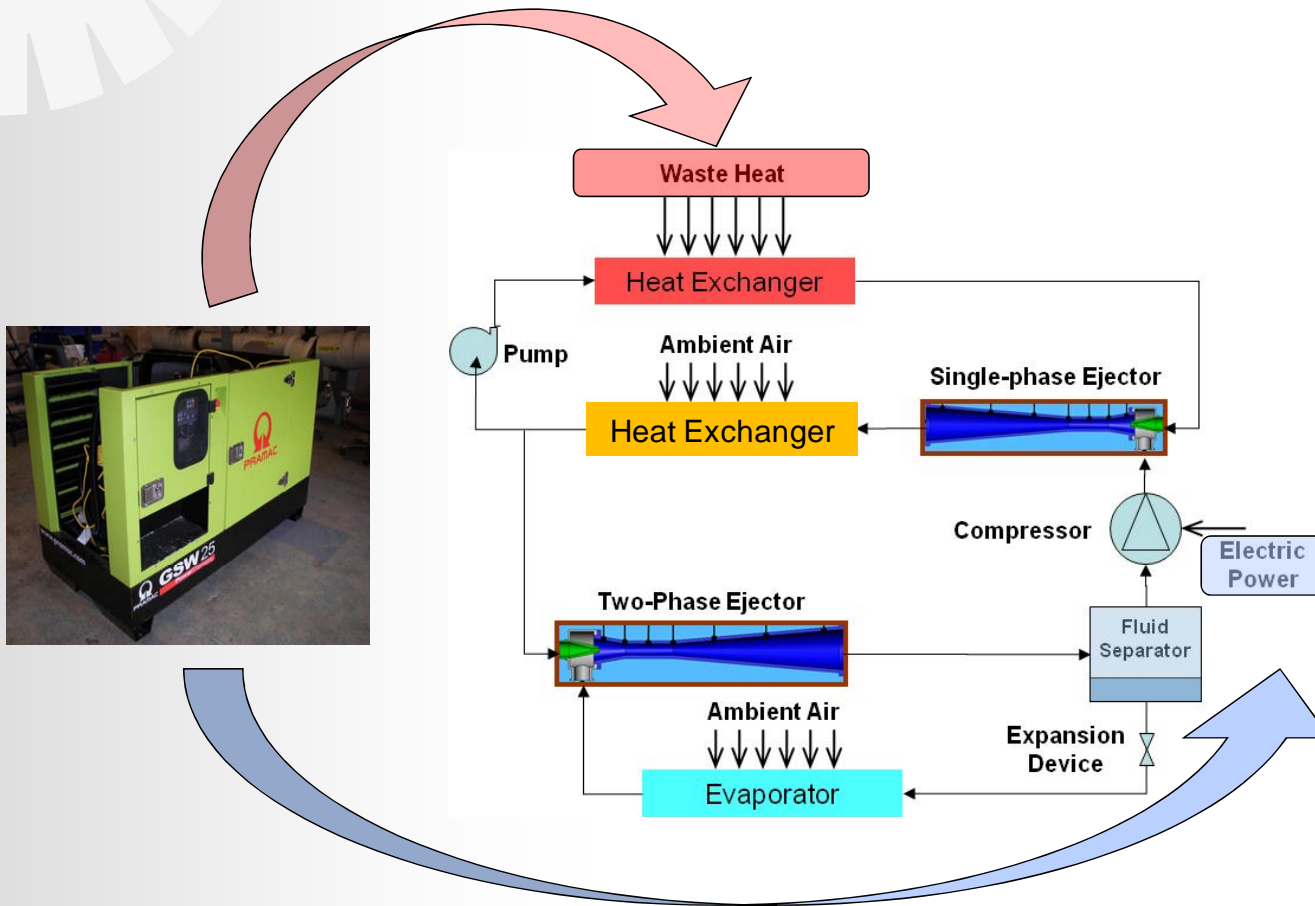
Fabrication and Testing: Advance Technology Demonstrator (ATD)

Plan

System Overview

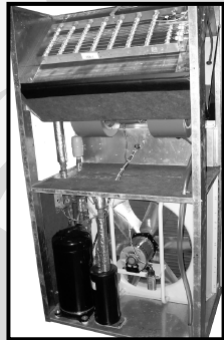
Objective: Design, develop & demonstrate a CO₂ 5TR (@ 125F ambient) environmental control unit (ECU) using ejector top & bottom cycles

Deliverables: +10% η_{system} vs. R410A (baseline); ATD; and reduced-order design tools

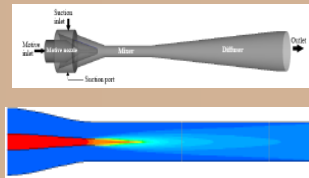


Development Process

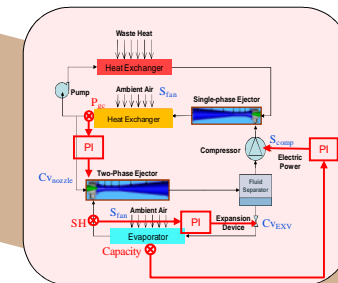
Model based process used to optimize system configuration and component design



✓ **Key System Requirements**
(Heat recovery; 125 F/90F)



✓ **Component Design & Analysis**



✓ **System Performance and Controls Analysis**



ATD and Models



Testing and Validation

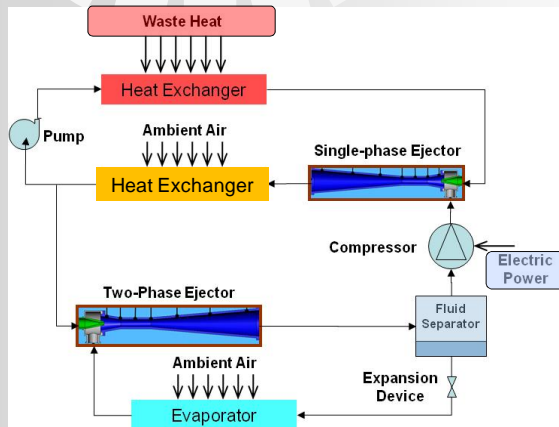


✓ **ATD fabrication and commissioning**

System and Component Design

Steady-state system model developed in EES and used to design components

System Modeling and Analysis

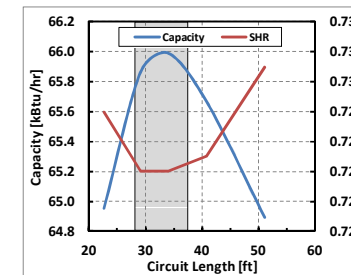


System Schematic

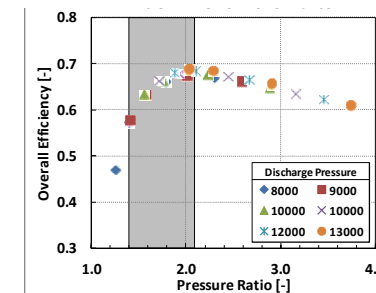
System modeled
in EES



Component Design



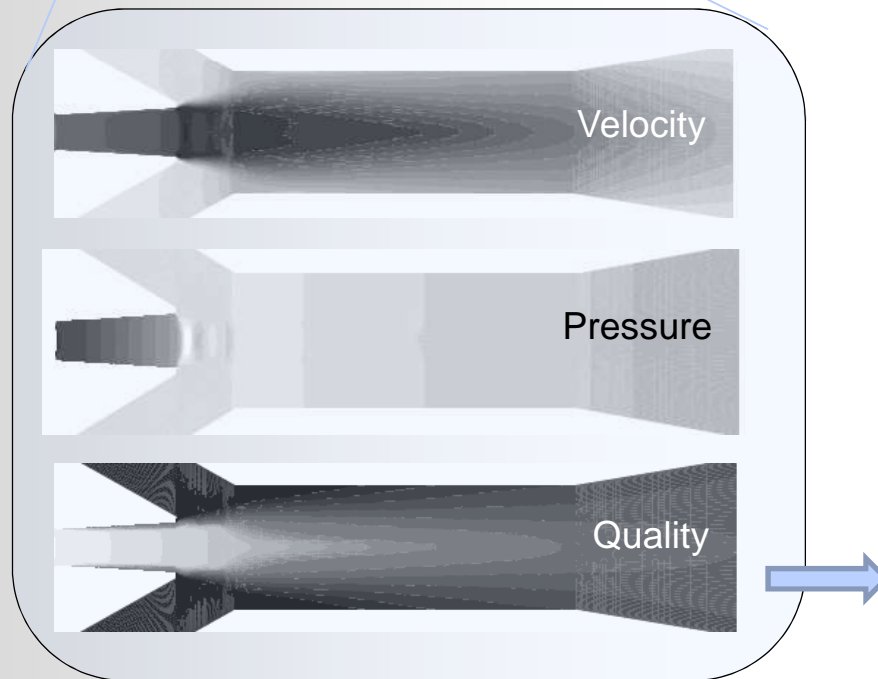
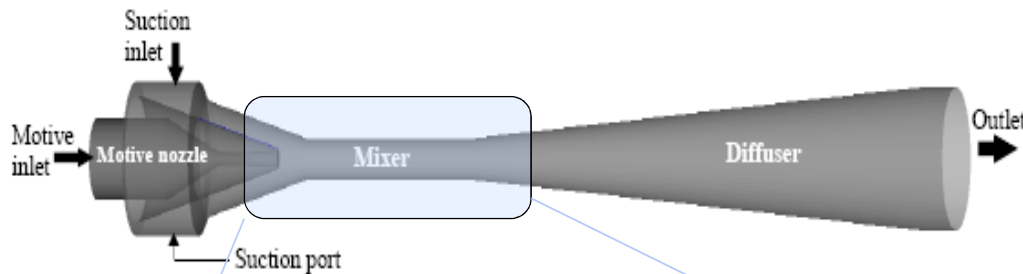
Heat Exchanger



Compressor

Work Recovery Ejector Design

Physics based CFD model developed and validated against multiple experimental data used to design work recovery ejector



Bubble growth: inertial and thermal

$$\dot{m}_{\text{cav},e} = C_e \frac{\sqrt{k}}{\sigma} \rho_l \rho_v \left[\frac{2}{3} \frac{P_v - P}{\rho_l} \right]^{1/2} (1 - \chi_v - \chi_g)$$

$$\dot{m}_{\text{boil}} = \pm \left[\frac{\hat{\sigma}}{2 - \hat{\sigma}} \right] \left(\frac{M}{2\pi R T_{\text{sat}}} \right)^{1/2} [P - P_v]$$

Drift-flux phase slip

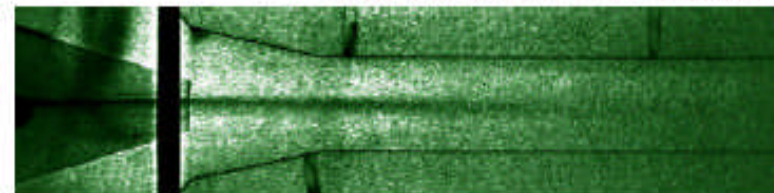
$$\mathbf{v}_{dr,p} = \mathbf{v}_{pq} - \frac{1}{\rho} \alpha_k (\rho \mathbf{v}_q)_k$$

2-phase sonic speed

$$\frac{1}{\rho c^2} = \frac{\alpha_v}{P} [(1 - \epsilon_v) f_v + \epsilon_v g_v] + \frac{1 - \alpha_v}{P} \epsilon_l g_l$$

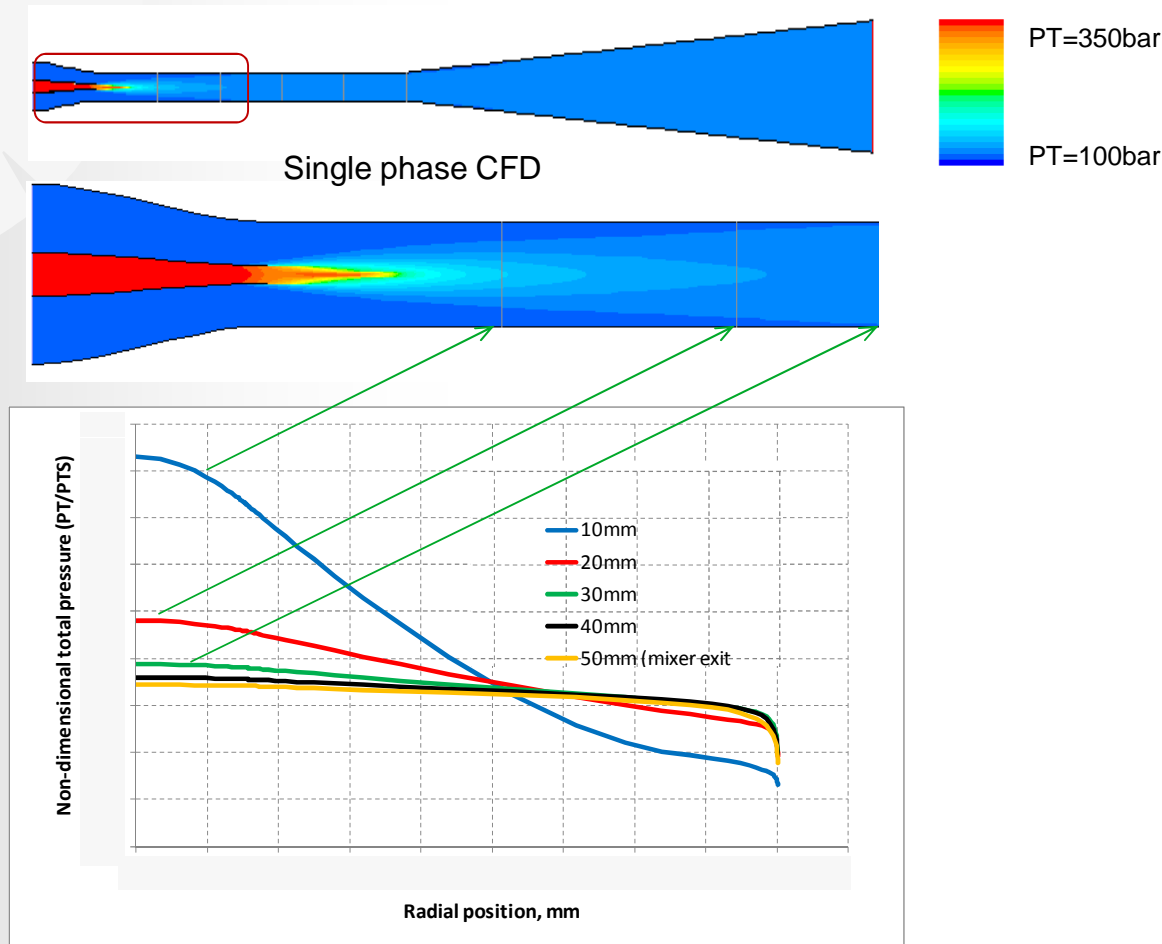
Model equations as published in International Journal of Heat and Mass Transfer (v.55, 2012)

Neutron image validation



Heat Recovery Ejector Design

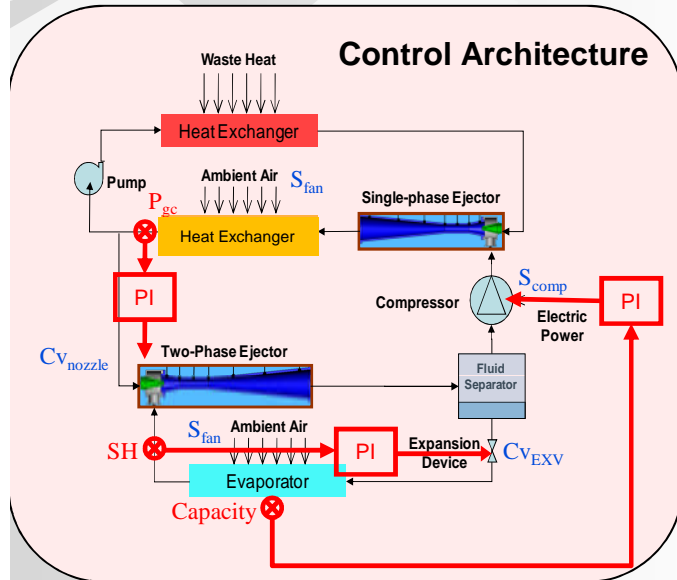
Mixing limits design but simulation can be used to investigate new alternatives



Motive momentum dissipates through turbulence too early in the mixing process when entrainment ratio is very high

Integrated Controls

Automatic synchronization of three loops to maximize system efficiency

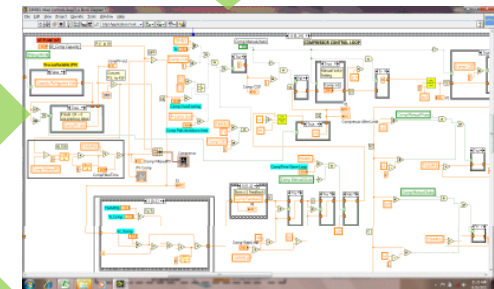


Actuator	Controlled variable
Compressor	Capacity
Ejector	Gas cooler pressure
EXV	Superheat
Gas cooler fan	Indirectly for COP

✓ **Component constraints**

✓ **Set points (EES, steady state)**

✓ **Controls tuning & closed-loop simulation**



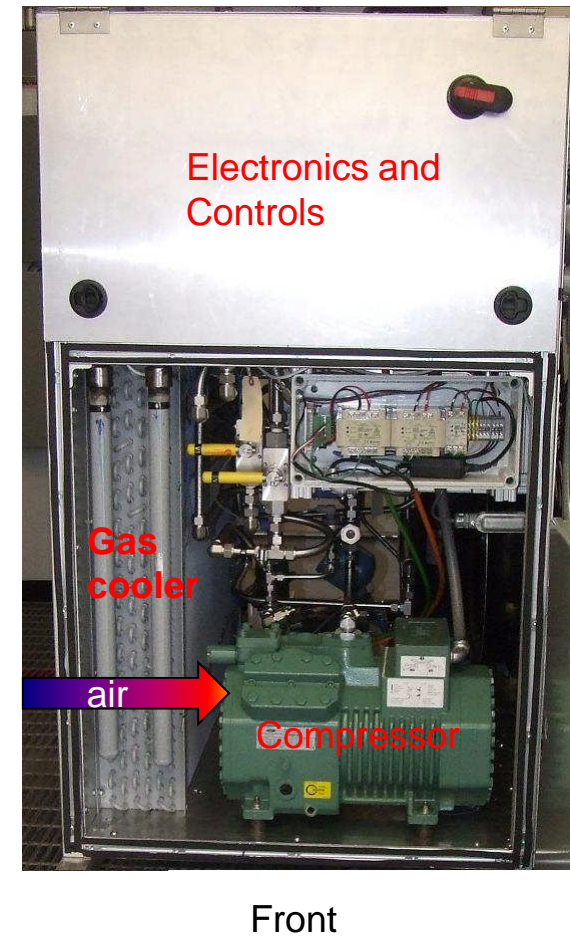
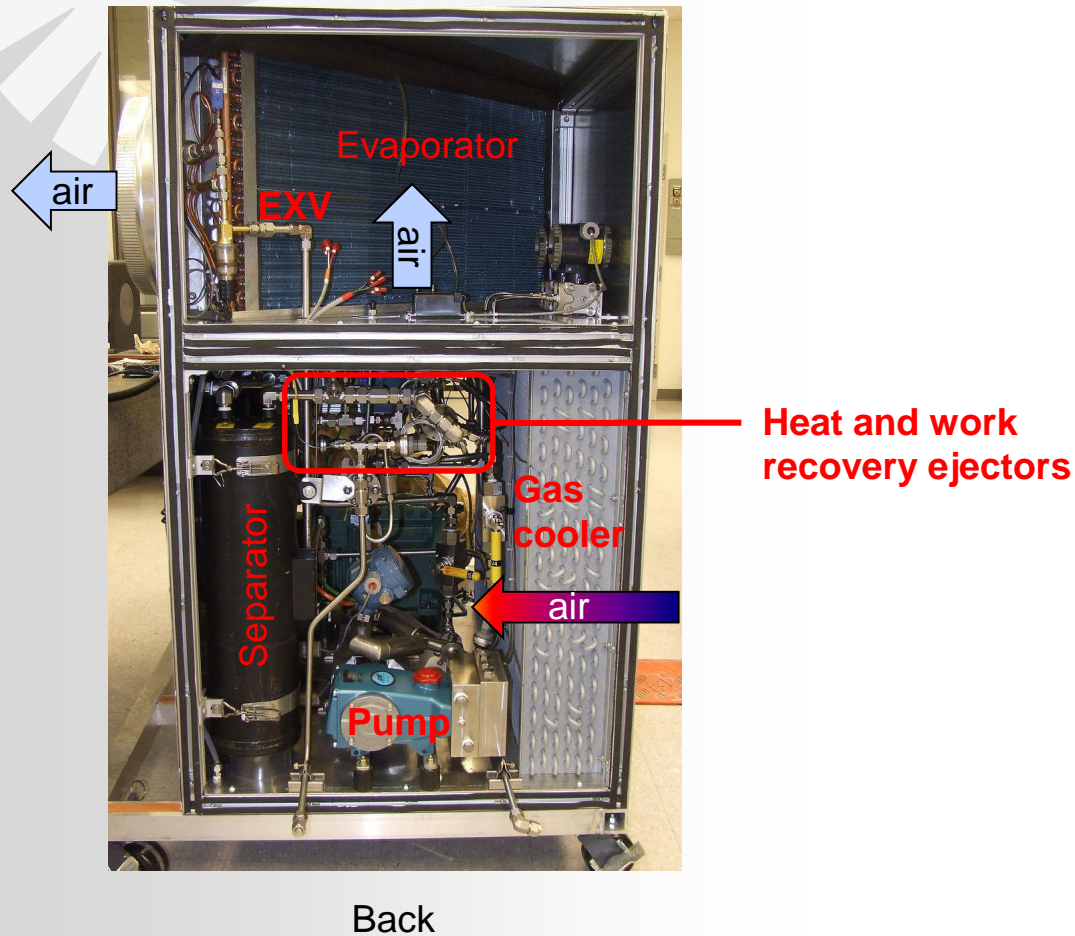
✓ **Implementation (LabView)**



✓ **Control Performance Verification**

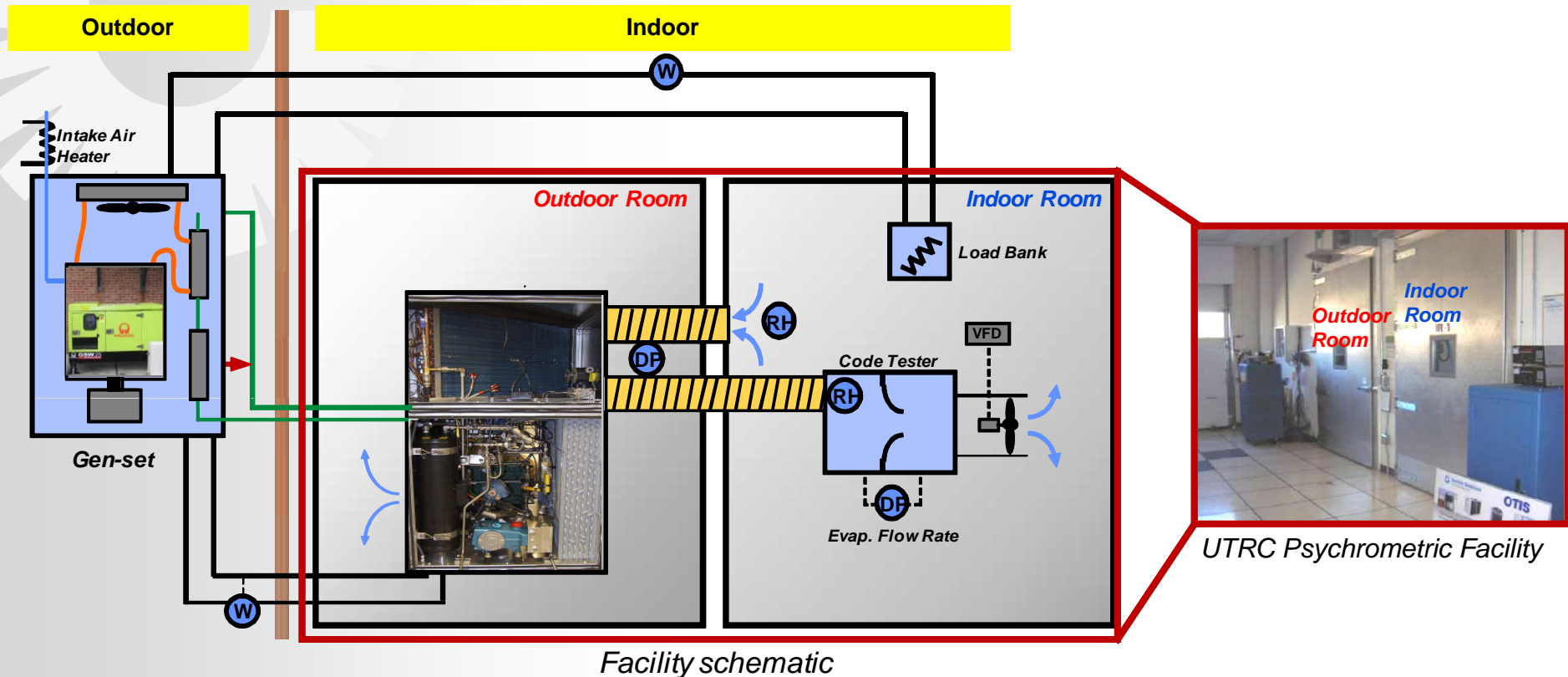
Advance Technology Demonstrator (ATD)

Advance technology demonstrator fabricated



Advance Technology Demonstrator (ATD)

ATD commissioned at Psychrometric Facility



Test Conditions for Indoor and Outdoor rooms

Test Conditions	Indoor Room		Outdoor Room
	Dry bulb (°F)	Dew Point (°F)	Dry bulb (°F)
ARI B	80	60.3	82
ARI A	80	60.3	95
Army 125	90	75	125

Tested 3 modes:

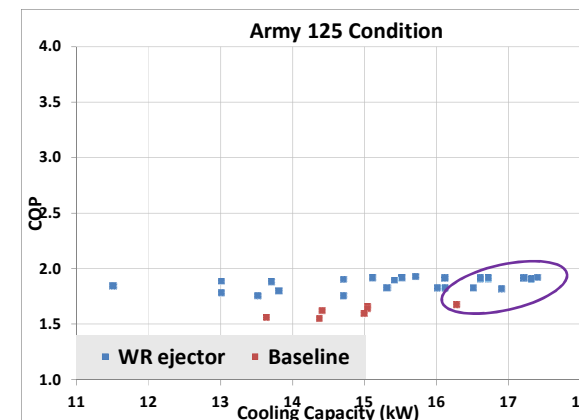
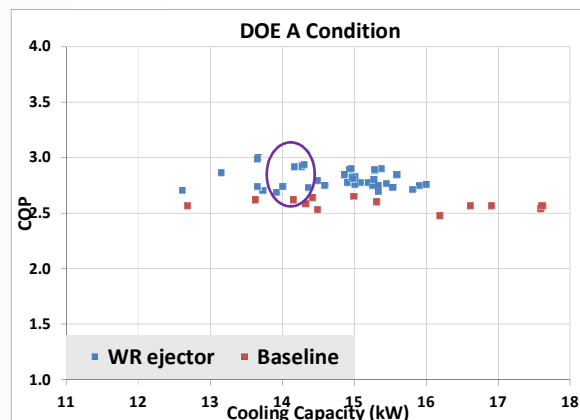
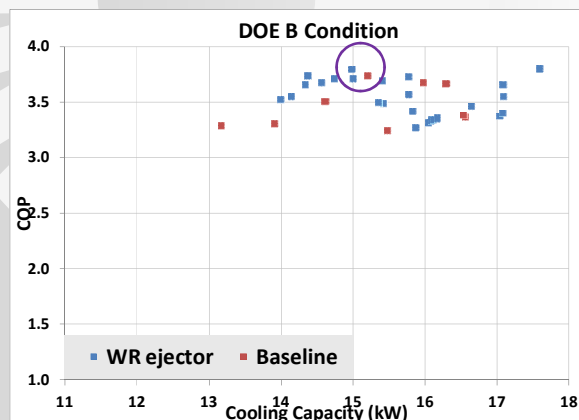
simple cycle, work recovery, work & heat recovery

Other tests include:

Low ambient and endurance/controls reliability

Test Results Summary

Up to 16% improvement in system efficiency demonstrated with work recovery ejector cycle



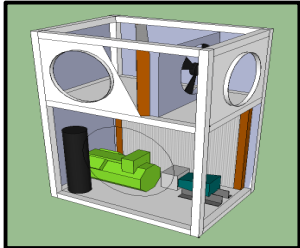


Condition		Cooling (kW)	System Efficiency (COP)	
			Testing (Measured)	
DOE B (82°F)	WR & HR	14.7	3.21	
	WR ejector	15.0	3.80	2% ↑
	Baseline	15.2	3.74	-
DOE A (95°F)	WR & HR	15.5	2.61*	
	WR ejector	14.3	2.93	11% ↑
	Baseline	14.4	2.65	-
Army (125°F)	WR ejector	17.4	1.93	16% ↑
	Baseline	15.0	1.66	-

Performance Metrics

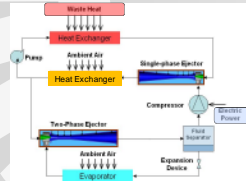
Performance: Demonstrated 2x COP improvement vs. current ECU but 30% short of target

Size: Current ATD comparable to existing ECU but exceeds targets. Optimized ATD weight within target

Name	Typical Current ECU	Contract Target	Current ATD	Improved ATD w/o Heat Recovery
System efficiency @ 125F	~1	2.75	1.93 (measured)	similar to current ATD
Size	39"x28"x72" 45.5 cu ft	36"x36"x48" 36 cu ft	32"x43"x57" 45.4 cu ft	32"x43"x50" 40 cu ft
Weight	<750 lbm	target 600 lbm (stretch 400 lbm)	934 lbm	< 500 lbm
				

Contract Plan

Demonstrated TRL 5 through advance technology demonstrator system testing



✓ Task 1: Hybrid Cycle Design

✓ Tasks 2&3: 1 and 2-Phase Ejector Modeling (CFD)



✓ Task 4: Reduced-Order Modeling

Q1

2010 Q2

Q3

Q4

2011 Q1

Q2

Q3

✓ Contract Signed

✓ Design Review

✓ CERDEC Review

✓ Final Report And Deliver ATD to Army

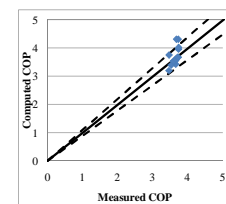


✓ Task 5: ATD fabrication/commissioning

✓ Task 6: Integrated Controls

- ✓ Model based control strategy
- ✓ Develop final control strategy (June. 2011)

✓ Task 7: System Testing and Modeling



Acknowledgement

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